## Philips Semiconductors B.V.

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# 2GHz LOW NOISE AMPLIFIER WITH THE BFG410W 

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#### Abstract

: This application note contains an example of a Low Noise Amplifier with the new BFG410W Double Poly RF-transistor. The LNA is designed for a frequency $f=2 G H z$. The Noise Figure NF~1.7dB at $f=2 \mathrm{GHz}$ and the gain $S_{21} \sim 14 d B$.


Appendix I: Schematic of the circuit
Appendix II: Printlayout and list of used components \& materials
Appendix III: Results of simulations and measurements

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## Introduction:

With the new Philips silicon bipolar double poly BFG400W series, it is possible to design low noise amplifiers for high frequency applications with a low current and a low supply voltage. These amplifiers are well suited for the new generation low voltage high frequency wireless applications. In this note a first study of such an amplifier will be given. This amplifier is designed for a working frequency of 2 GHz .

## Designing the circuit:

The circuit is designed to show the following performance:
transistor: BFG410W
$\mathrm{V}_{\mathrm{ce}}=2 \mathrm{~V}, \mathrm{l}_{\mathrm{c}}=2 \mathrm{~mA}, \mathrm{~V}_{\mathrm{SUP}} \sim 3.3 \mathrm{~V}$
freq $=2 \mathrm{GHz}$
Gain~14dB
$\mathrm{NF}<=1.7 \mathrm{~dB}$
VSWRi<1:2
VSWRo<1:2
In the simulations the effect of extra RF-noise caused by the SMA-connectors was omitted, so in the practical situation the NF is $\sim 0.1 \mathrm{~dB}$ higher. This LNA is not optimised for the highest IP3. The IP3 can be optimised by:
I. an extra series RC-decoupling of the base to the ground
II. increasing $\mathrm{I}_{\mathrm{c}}$

With the solution I. two extra components are necessary, and with solution II, the Noise Figure of the LNA increases and the optimum source impedance also.

The in- and outputmatching is realised with a LC-combination. Also extra emitter-inductance on both emitterleads ( $\mu$-strips) are used to improve the matching and the Noise Figure.

## Designing the layout:

A lay-out has been designed with HP-MDS. Appendix II contains the printlayout.

## Measurements:

Simulations (with realistic RF-models of al used parts) and measurements of the total circuit (epoxy PCB) are done (Appendix III).

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Appendix I: Schematic of the circuit


Figure 1: LNA circuit
2 GHz LNA Component list:

| Component: | Value: | Comment: |
| :---: | :---: | :---: |
| R1 | $47 \mathrm{~K} \Omega$ | Bias. |
| R2 | $10 \Omega$ | Better RF-stability (K>1). |
| R3 | $22 \Omega$ | RF-block. |
| R4 | $560 \Omega$ | Cancelling $\mathrm{H}_{\text {FE- }}$-spread. |
| C1 | 1 pF | Input match. |
| C2 | 5.6 pF | 2 GHz short. |
| C3 | 5.6 pF | 2GHz short. |
| C4 | 1 nF | RF-short |
| C5 | 3.3 pF | Output match. |
| C7 | 0.47 pF | Better RF-stability ( $\mathrm{K}>1$ ). |
| $\mu \mathrm{s} 1$ | $\mathrm{W}=0.25 \mathrm{~mm}$ | $\mu$-stripline $\mathrm{Z}_{0} \sim 95 \Omega$ (PCB: $\varepsilon_{\mathrm{r}} \sim 4.6, \mathrm{H}=0.5 \mathrm{~mm}$ ) |
| $\mu \mathrm{s} 2$ | $\mathrm{W}=0.25 \mathrm{~mm}$ | $\mu$-stripline $Z_{0} \sim 95 \Omega$ (PCB: $\left.\varepsilon_{r} \sim 4.6, \mathrm{H}=0.5 \mathrm{~mm}\right)$ |
| $\mu \mathrm{s} 3$ | $\mathrm{W}=0.25 \mathrm{~mm}$ | $\mu$-stripline $Z_{0} \sim 95 \Omega$ (PCB: $\varepsilon_{r} \sim 4.6, \mathrm{H}=0.5 \mathrm{~mm}$ ) |
| $\mu \mathrm{s} 4$ | (next table) | Emitter induction: $\mu$-stripline + via |

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$\mu$ S4 Emitter induction ( $\mu$-stripline + via):

| Name | Dimension | Description |
| :--- | :--- | :--- |
| L1 | 2.0 mm | length $\mu$-stripline; $\mathrm{Z}_{0} \sim 48 \Omega \quad\left(\mathrm{PCB}: \varepsilon_{\mathrm{r}} \sim 4.6, \mathrm{H}=0.5 \mathrm{~mm}\right)$ |
| L2 | 1.0 mm | length interconnect stripline and via-hole area |
| L3 | 1.0 mm | length via-hole area |
| W1 | 0.5 mm | width $\mu$-stripline |
| W2 | 1.0 mm | width via-hole area |
| D1 | 0.4 mm | diameter of via-hole |

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Appendix II: Printlayout and list of used components \& materials


2 GHz LNA
BFG410W

Figure 2: Printlayout
2GHz LNA Component list:

| Component: | Value: |  |
| :--- | :--- | :--- |
|  | size: |  |
| R1 | $47 \quad \mathrm{~K} \Omega$ | 0603 Philips |
| R2 | $10 \quad \Omega$ | 0603 Philips |
| R3 | $22 \quad \Omega$ | 0603 Philips |
| R4 | $560 \quad \Omega$ | 0603 Philips |
| C1 | $1 \quad \mathrm{pF}$ | 0603 Philips |
| C2 | 5.6 pF | 0603 Philips |
| C3 | 5.6 pF | 0603 Philips |
| C4 | $1 \quad \mathrm{nF}$ | 0603 Philips |
| C5 | 3.3 pF | 0603 Philips |
| C5 | $0.47 \quad \mathrm{pF}$ | 0603 Philips |
| PCB | $\varepsilon_{\mathrm{r}} \sim 4.6, \mathrm{H}=0.5 \mathrm{~mm}$ | FR4 |

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Appendix III: Results of simulations and measurements:
BFG410W, Vsup $=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{CE}}=2 \mathrm{~V}, \mathrm{I}_{\mathrm{C}}=2 \mathrm{~mA}$ :

|  | HP-MDS <br> Simulation: <br> S-par. | HP-MDS <br> Simulation: <br> SPICE- <br> model | Measurements <br> PCB: | Comment: |
| :--- | :--- | :--- | :--- | :--- |
| $\mid$ S21 $\left.\right\|^{2}[\mathrm{~dB}]$ | 14.2 | 14.6 | 14.3 |  |
| $\mid$ S12 $\left.\right\|^{2}[\mathrm{~dB}]$ | -24.6 | -27.4 | -29.5 |  |
| VSWRi | 2.6 | 2.1 | 2.2 |  |
| VSWRo | 1.3 | 1.3 | 2.1 |  |
| Noise Figure [dB] | 1.6 | 1.8 | 1.7 |  |
| IP3 $[\mathrm{dBm}]$ (output) | - | - | - | not measured |

Figure 3: HP-MDS simulation circuit


