

AN13453

Card coil design notes for MIFARE Ultralight AES

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Document information

Information	Content
Keywords	Contactless, MIFARE Ultralight AES, ISO/IEC 14443, Resonance, Frequency, Coil, Inlay
Abstract	This document provides guidance for engineers designing loop antenna coils for MIFARE Ultralight AES.



Revision history

Revision history

Rev	Date	Description
1.2	20220420	Corrected typos, editorial changes, removed unnecessary figure
1.1	20220218	Security status changed to "Company public"
1.0	20220208	Initial version

1 Introduction

MIFARE Ultralight AES (later called PICC, Proximity Integrated Circuit Card), a passive device (without battery) is powered by magnetic field generated by a PCD (Proximity Coupling Device). To get the magnetic flux cut by the PICC, it also requires a loop antenna. A PICC with connected coil antenna is also called transponder.

This document describes some notes to the design of such loop antennas for MIFARE Ultralight AES.

The detail loop antenna design is explained in [\[1\]](#). Although such antennas are relatively straightforward in principle and look very similar when comparing various contactless smartcards, experience proves that their parameters do have a noticeable impact on performance.

In this document, some examples are attached for your reference, but it is recommended to verify them before starting production. In addition, customers who want to reuse existing MIFARE product-based card coil antenna design or design a completely new antenna can also get information as to what considerations to make.

1.1 How to use this document

In this document only the hints and notes specific to MIFARE Ultralight AES are explained. All the basics and design details are explained in [\[1\]](#). Please use [\[1\]](#) as the base document and apply wherever requires the notes mentioned here.

1.2 Terms and abbreviations

Table 1. Abbreviations

Acronym	Description
AES	Advanced Encryption Standard
PCD	Proximity Coupling Device
PICC	Proximity IC Card

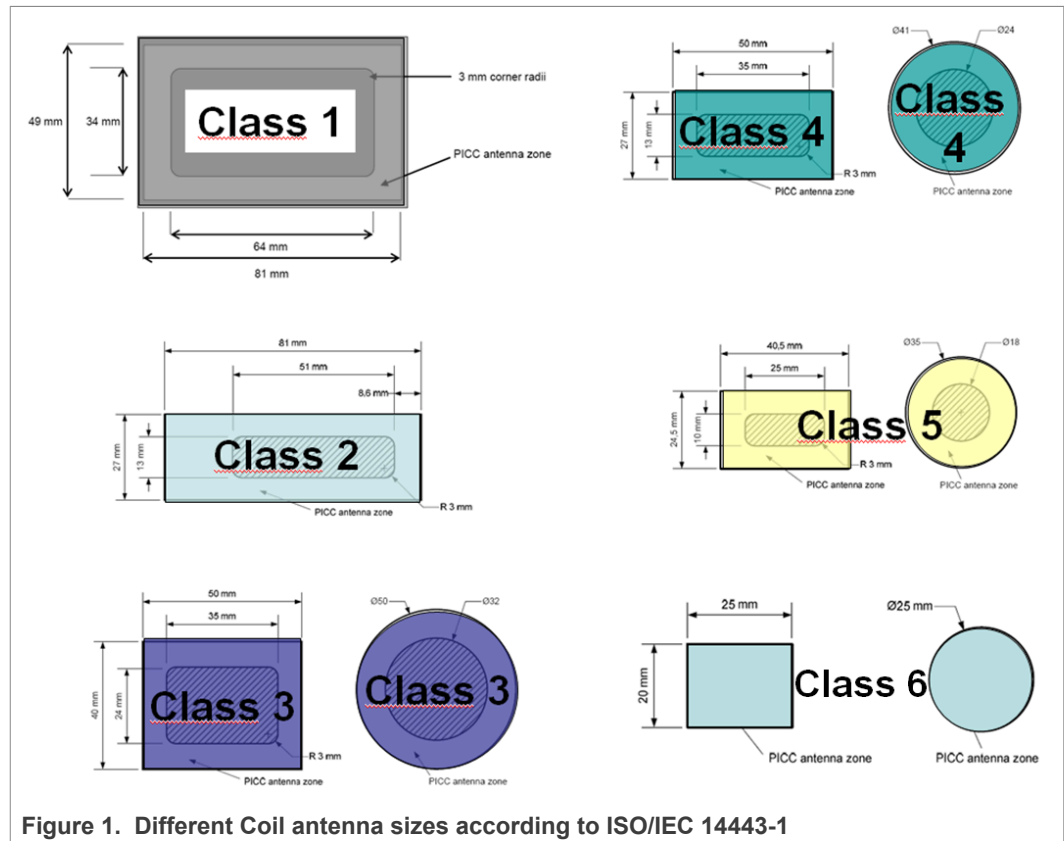
2 Card Coil design notes for MIFARE Ultralight AES

There are different classes of antennas defined in the ISO/IEC 14443-1 / Amd. 1, which feature different antenna sizes. These antenna classes may be used in contactless application for the MIFARE Ultralight AES PICC. For different antenna classes, the design of PICC coils is different. Even different application requirements also lead to different antenna designs.

Basically, three parameters are important for the card coil design: coil area, coil quality factor, and the resonance frequency of the transponder under loaded conditions.

2.1 Different classes of antennas according to ISO/IEC 14443-1

In [Figure 1](#) different antenna sizes according to ISO/IEC 14443-1[2010] are shown.



2.2 Card coil area

Make the card coil area as large as possible. Bending corners are better than sharp corners.

2.3 Coil Q-factor

To get optimum performance and to cover manufacturing tolerances, for MIFARE Ultralight AES, the recommended coil Q values are given in [Table 2](#).

2.3.1 Measurement of Coil Q-factor

There are different ways to measure the Q-factor of the coil, which may end up with different results. It is recommended to follow the way described in the Card Coil Design Guide [\[1\]](#) or get help from your NXP technical support.

2.4 Definition for “unloaded” and “loaded” conditions.

“**loaded conditions**”, or just “loaded”, means that the MIFARE Ultralight AES chip gets enough power to be able to fully operate. With the NXP setup used (defined in [\[2\]](#)), those conditions are achieved, when the power at the network analyzer output is set to the value of +10 dBm.

“**unloaded conditions**”, or just “unloaded”, means that the MIFARE Ultralight AES chip does not get enough power in order to even start to operate. With the NXP setup used (defined in [\[2\]](#)), those conditions are achieved, when the power at the network analyzer output is set to the value of -30 dBm.

Both conditions were created with an NXP dedicated measurement setup, which is described in [\[2\]](#). All measurement results presented further down in this document have been obtained with this setup and under “loaded” and “unloaded” conditions as defined earlier in this paragraph.

2.5 Loaded resonance frequency of the transponder

The loaded resonance frequency of the transponder is the resulting resonance frequency, if the IC is operated under loaded conditions.

In general, the appropriate resonance frequency of the transponder depends on the card ICs and applications. To get optimum performance and to cover manufacturing tolerances, for MIFARE Ultralight AES, use the recommended loaded resonance frequency given in [Table 2](#).

2.5.1 Measurement of loaded resonance frequency of the transponder

There are different ways to measure the resonance frequency of the transponder, which may end up with different results. It is recommended to follow the way described in the Card Coil Design Guide [\[2\]](#) or get help from your NXP technical support.

2.6 NXP recommendation for PICC coil design

[Table 2](#) summarizes the recommendations for the PICC coil design.

Note the following points applicable to the 17 pF chip version:

- MIFARE Ultralight AES works best between 13.56 - 16 MHz loaded fres.
- For maximum operating distance, the loaded fres is ideally close to 14.5 MHz.
- A loaded fres too close at 13.56 MHz (e.g 14.00 MHz) might detune the reader antenna and result in reading issues on some PCDs.

Table 2. PICC coil design recommendation

Antenna class	Recommended variant of MIFARE Ultralight AES	Recommended loaded transponder resonance frequency (f_R)	Recommended Coil Q	Comments
Class 1	17 pF	13.56 MHz < f_R < 16 MHz	> 30	Transponder optimum loaded resonance frequency for single card operation is close to 14.5 MHz. Transponder optimum loaded resonance frequency for stacked 2 cards operation is close to 15.5 MHz.
Class 2	50 pF	13.56 MHz < f_R < 14.50 MHz	> 40	The optimum loaded resonance frequency is slightly above 13.56 MHz.
Class 3	50 pF	13.56 MHz < f_R < 14.50 MHz	> 40	The optimum loaded resonance frequency is slightly above 13.56 MHz.
Class 4	50 pF	13.56 MHz < f_R < 14.50 MHz	> 40	The optimum loaded resonance frequency is slightly above 13.56 MHz.
Class 5	50 pF	13.56 MHz < f_R < 14.50 MHz	> 40	The optimum loaded resonance frequency is slightly above 13.56 MHz.
Class 6	50 pF	13.56 MHz < f_R < 14.10 MHz	> 40	The optimum loaded resonance frequency is slightly above 13.56 MHz.

Those recommended quality factor values for the coil are important to get a good power transfer and to increase the so called power range of the transponder.

For class 1 antennas (17 pF IC version), a minimum Coil Q-factor of 30 is recommended. The resulting transponder Q-factor under “unloaded” conditions is similar to this value. Once the PICC starts to operate, its (loaded) Q-factor is decreasing and this is leading to a loaded Q-factor in the range of 8-9. This value is in the middle of the range of 6-15, which results in a good performance.

All those considerations are valid for class 2 to class 6 antennas (50 pF IC version) a minimum coil Q-factor of 40 is recommended.

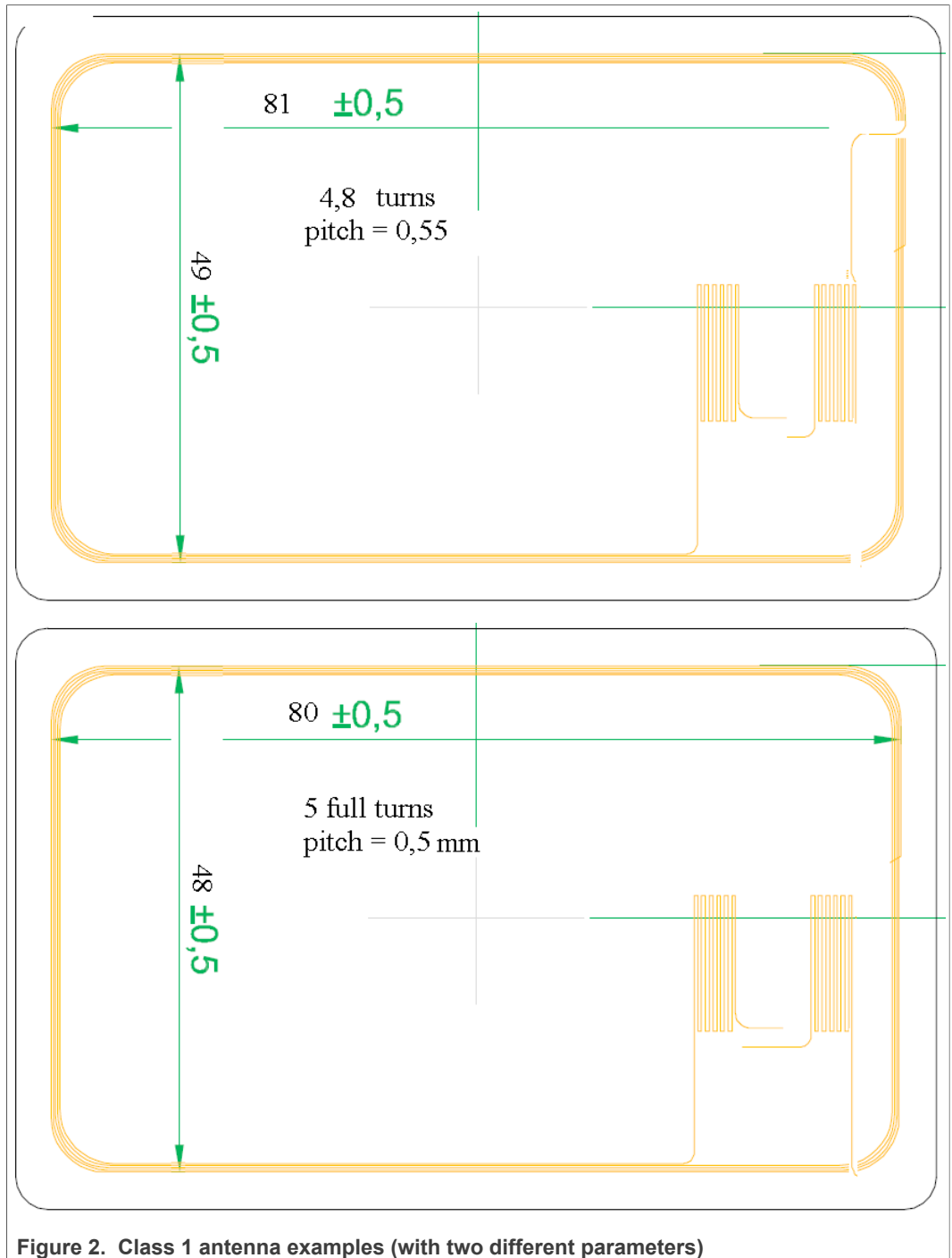
Please check [Section 2.9.1](#) in this document for further reference on this topic.

2.7 Antenna design hints and recommendations for 17 pF chip

2.7.1 ID1-sized wired antennas

Hints for antenna design

- Within the confines of the application and the card manufacturing processes used, try to maximize the antenna size. The outermost turn of the antenna coil should be placed as close as possible to the edge of the area represented by an 81 x 49 mm rectangle. Class 1 antenna examples (with two different parameters) are shown in [Figure 2](#).
- **Note:** International standards and industry specifications may restrict the choice of the maximum allowed antenna coil size.



For ID1 size (class 1) antennas, the 17 pF chip version is recommended. For all other classes, the usage of the 50 pF version of the MIFARE Ultralight AES PICC is recommended.

2.7.2 ID1-sized etched antennas

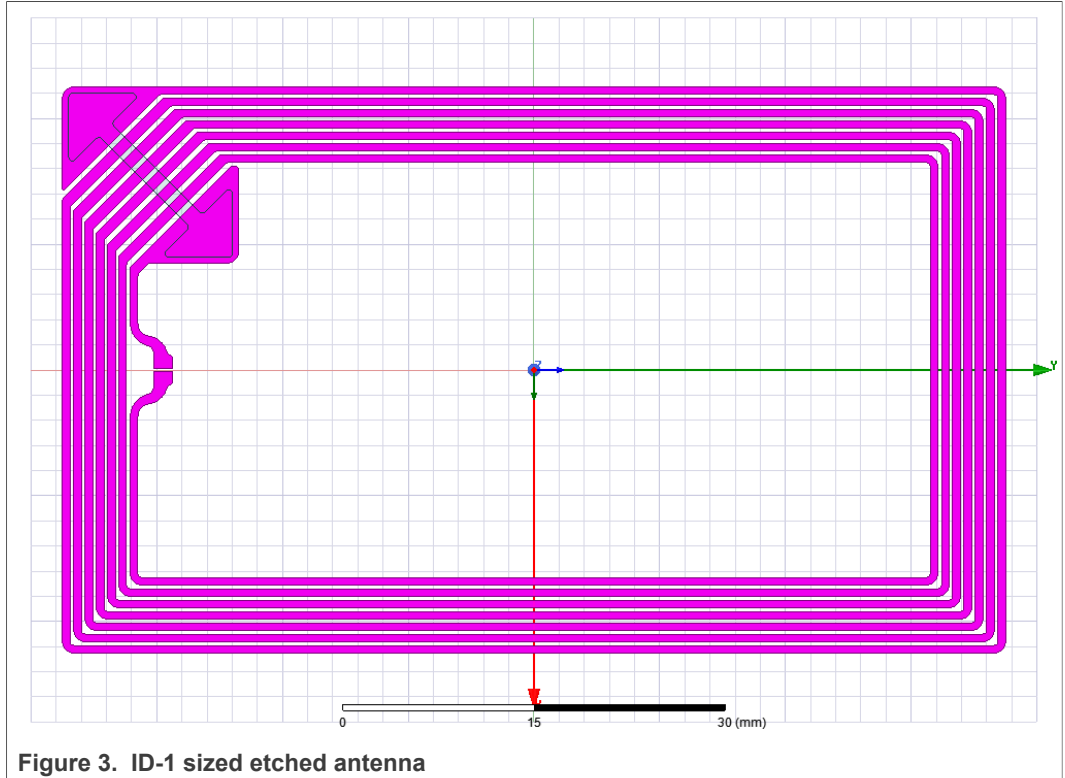


Figure 3. ID-1 sized etched antenna

An etched antenna coil (typical made of copper/aluminium on polyester) may be used as well. [Figure 3](#) shows a 7-turn antenna with a dimension of 75 x 45 mm.

- Track width, $w = 0,6$ mm
- Gap between tracks, $g = 0,3$ mm
- Track thickness (coil): $t_{coil} = 0,03$ mm
- Track thickness (bridge): $t_{coil} = 0,01$ mm
- Number of Turns, $N = 7$
- Carrier Material: Polyester
- Carrier Thickness: 0.038 mm
- Carrier Er: 3.2

Above mentioned parameters will together with a MIFARE Ultralight AES 17 pF result in a loaded f_{RES} of ~ 15.0 MHz.

2.8 Practical design hints and recommendations for 50 pF chip

For class 2 and up to class 6 antennas, it is recommended to use 50 pF chip version.

2.8.1 Round etched antennas

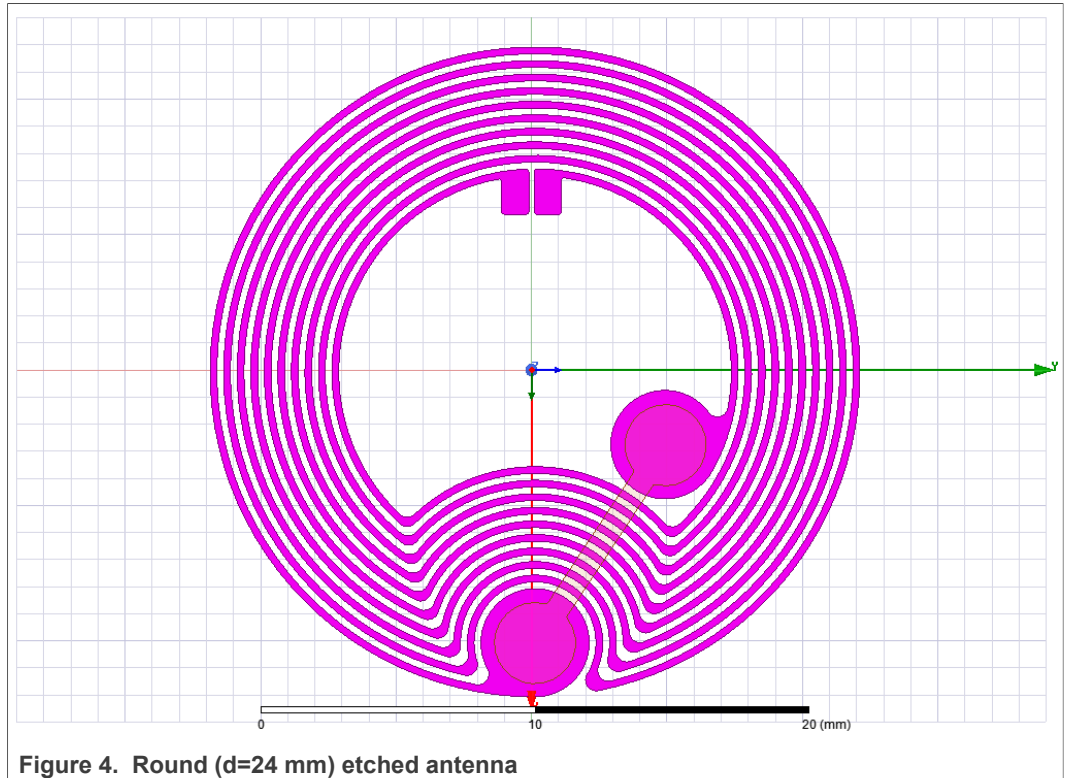


Figure 4. Round (d=24 mm) etched antenna

Figure 4 shows a small antenna design for the MIFARE Ultralight AES 50 pF.

- Track width, $w = 0,25$ mm
- Gap between tracks, $g = 0,25$ mm
- Track thickness (coil): $t_{\text{coil}} = 0,03$ mm
- Track thickness (bridge): $t_{\text{coil}} = 0,01$ mm
- Number of Turns, $N = 10$
- Carrier Material: Polyester
- Carrier Thickness: 0.038 mm
- Carrier Er: 3.2

Above mentioned parameters will together with a MIFARE Ultralight AES 50 pF result in a loaded f_{RES} of ~ 14.0 MHz.

2.9 Antenna coil design considerations for unloaded and loaded conditions

2.9.1 Quality factor and bandwidth of the transponder

The quality factor of a transponder Q_T is an important parameter defined at air interface. The value of Q_T has to be properly chosen in order to guarantee sufficient performance for both power and data transmission.

The quality factor of the transponder results from the quality factor values of its' both components, the antenna (Q_A) and the chip (Q_C). It is determined by the component with lower Q-factor, in this case by the Q_C . Taking into account that both chip electrical parameters (capacitance C_C and resistance R_C) are power and frequency dependent, it is obvious that the Q_T also changes with power and frequency. This point is relevant when considering Q_T both under "loaded" and "unloaded" conditions.

For a transponder resonant LCR circuit, Q_T can be determined in frequency domain. Q_T is related to the bandwidth, which can be measured from the resistance curve as shown in [Figure 5](#). [3].

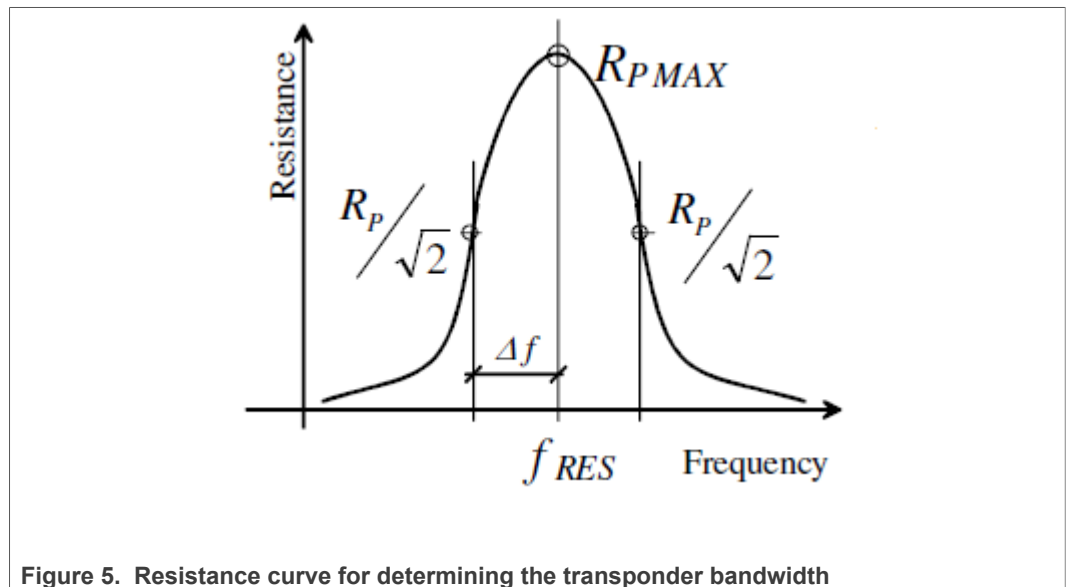


Figure 5. Resistance curve for determining the transponder bandwidth

Q_T can be calculated by using formula [Equation 1](#).

$$Q_T = \frac{f_{res}}{2\Delta f} = \frac{f_{res}}{B} \tag{1}$$

Where f_{res} is a transponder resonance frequency and Δf is defined in [Figure 5](#).

2.10 Required transponder bandwidth for (PICC -> PCD) data transfer

The demand for data transfer sets requirements on the transponder bandwidth B , which limits the transponder quality factor Q_T . The needed bandwidth is related to the modulation scheme, coding and data rates used.

The theoretical required bandwidth for 106 kbit/s is 1.8 MHz . Detailed explanation can be found in [\[4\]](#).

Important remark: If a transponder bandwidth is smaller than theoretically required, it does not automatically mean that the communication will not be possible. What will happen is that the sideband levels of the card answer will be damped more than 3 dB (which was accepted for a classical definition of bandwidth), but might be still sufficient for successful communication.

Note for higher antenna classes (class 2 to class 6): With coil size reduction the inductance of the coil decreases. Additionally, there is a recommendation to utilize the 50 pF IC version together with antennas smaller than class 1. This results in the increase of the transponder Q_T factor ($Q_T = R_p * \sqrt{C_p / L}$). It is recommended to check the resulting Q_T or bandwidth B of a newly designed transponder, to enable successful communication.

2.11 Operation with stacked cards

If more than one card is on the reader, then the system resonance frequency will reduce, which causes the energy transfer between cards and reader to be reduced. Therefore the reading distance will get reduced as well. In order to compensate for that, one can tune the card to a higher resonance frequency. However, this will result in a worse performance in single card operation.

For the stacked card use case, it is recommended to tune the card to around 16.5 MHz to allow the resonance frequency of the stacked card system not to fall significantly below 13.56 MHz and therefore optimize for stacked cards operation. Attention: H_{min} for single card operation will be higher if the resonance frequency is at 16.5 MHz.

3 References

- [1] AN11093 Card Coil Design Guide, available in [Secure Files on NXP.com](#), secure files number: AN0117**¹
- [2] PICC and VICC Resonance Frequency Measurement
- [3] M. Gebhart, Air Interface, Antennas and Signals in Contactless Near-Field Communication 2nd lecture in Selected Topics of Advanced Analog Chip Design, 439.224
- [4] ISO/IEC 14443-3 Identification cards — Contactless integrated circuit cards — Proximity cards - Part 3: Initialization and anticollision

1 ** document version number

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